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Characterization and measurement

- Introduction
- Destructive methods
- Non-destructive methods
 - -Elastic wave method
 - -Infrared thermal method
 - -Non-contact resistivity method
 - -Dynamic modulus method
 - -Ellipse ring for crack sensitivity

Introduction

Destructive test – *obtain the* material properties by seriously destroying sample Nondestructive test – *obtain the* information without damaging samples

Introduction-destructive methods

Compression test
Tension test
Bending test
Impact test

Introduction-nondestructive

Quality control

- Finished products
- Injection of grout
- Position of reinforcing steel
- Welding of reinforcing steel
- Hydration rate of fresh concrete
- Selection of watermelon and eggs

Introduction-nondestructive

- b. In-service inspection
 - Boiler and vesile safety monitoring
 - Bridge safety monitoring
 - Building finish monitoring
 - Airplane

- Control methods for strength test

Open Loop Control (OLC)Close Loop Control (CLC)



- Calibration of transducers (1)

- a. Mechanical parameters: Displacement, Strain, Crack opening, Force
- b. Electric parameters: Voltage, Capacity, Impedance, Current

c. Calibration:

- Find relationship between electrical variables and mechanical variables
- General procedures
 - Connect the transducer to be calibrated
 - Provide a known mechanical parameter output
 - Adjust the reading of transducer to a desired value

- Calibration of transducers (2)

c. Calibration

e.g. A displacement transducer of 2.5mm full range



- Calibration of transducers (3)

Transducer



Destructive tests- Compressive test (1)

A set-up for compression test



Destructive tests- Compressive test (2)

Typical load versus axial displacement and load versus circumferential Displacement curves for three classes for concrete



Destructive tests – Tension test





Destructive tests – Tension test



Nondestructive test

-Shear wave reflection method



Principle of Shear Wave Reflection Method



Case 1: concrete is liquid

no wave transmission at interface

Principle of Wave Reflection



Case 2: concrete is hardening

transmission losses at interface



Typical Reflection Loss Development



Phase 1: liquid concrete → no reflection loss

Phase 2: concrete hardens \rightarrow attenuation increases

Phase 3: hardening continues → attenuation approaches final value

Point A – Initial Setting



vs. Strength К











Result of Field Test







Pulse Velocity

Determination

Relationships





Experimental Setup



Embedded sensor





Dynamic modulus and Poison's ratio

$$E = \rho C_L^2$$
 $\upsilon = \frac{C_L^2}{2C_T^2} - 1$

Where,

 C_L and C_T are longitudinal and transverse velocities, respectively. P is the density of the concrete specimen.

The calculated result fit well with the dynamic Young' modular measured by standard method.

Hydration monitoring using embedded sensor



Hydration monitoring using embedded sensor



 \checkmark In situ and real time monitoring

✓ Life time healthy monitoring



AE technique

AE technique is a passive NDT method. It relies on the detection of elastic waves generated by sudden release or change of energy or deformation in materials.

AE technique

- Active movement of defects
- whole structure
- highly sensitive
- on-line monitoring



聲發射測試技術



A acoustic wave propagation
Basic AE measurement system



AE technique



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AE Technique



Occurrence of AE rate during the tension test

AE technique



For 3-D case

$$e_{1i} = \sqrt{(x - x_1)^2 + (y - y_1)^2 + (z - z_1)^2} - \sqrt{(x - x_i)^2 + (y - y_i)^2 + (z - z_i)^2} - \Delta t_{1i}C$$

Sum of the square of the errors

$$e = \sum_{i=2}^{n} (e_{1i})^{2}$$
$$= \sum_{i=2}^{n} (d_{1} - d_{i} - \Delta t_{1i}C)^{2}$$

Differential with respect to x, y, z and C are in forms of;

$$f_{x}(x,y,z,C) = \frac{\partial e}{\partial x}$$
$$= 2\sum_{i=2}^{n} \left(\frac{x-x_{1}}{d_{1}} - \frac{x-x_{i}}{d_{i}}\right) (d_{1} - d_{i} - \Delta t_{1}iC)$$

$$f_{y}(x,y,z,C) = \frac{\partial e}{\partial y}$$
$$= 2\sum_{i=2}^{n} \left(\frac{y-y_{1}}{d_{1}} - \frac{y-y_{i}}{d_{i}}\right) (d_{1} - d_{i} - \Delta t_{1}iC)$$

$$f_{z}(x,y,z,C) = \frac{\partial e}{\partial z}$$
$$= 2\sum_{i=2}^{n} \left(\frac{z-z_{1}}{d_{1}} - \frac{z-z_{i}}{d_{i}}\right) (d_{1} - d_{i} - \Delta t_{1}iC)$$

$$f_{C}(x, y, z, C) = \frac{\partial e}{\partial C}$$
$$= 2\sum_{i=2}^{n} \Delta t_{1i} (\Delta t_{1i}C + d_{i} - d_{1})$$



AE events during period between pre 0.0 to 0.8 peak load



AE events during period after post 0.8 peak load



AE events during period between pre 0.0 to post 0.8 peak load



Major crack position for concrete specimen C-M13

Accelerated corrosion test



Comparison of AE and Galvanic measurement results





FIGURE 3b - AE Signal at the Three Transducers for a Single AE Event



Computation of corrosion position



$$(L-x)-x = \Delta t \cdot C$$
$$L-2x = \Delta + C$$
$$x = \frac{L-\Delta t C}{2}$$

Experimental Results

Location of AE Sources





Infrared thermograph --Introduction (1)

a) Light

An electromagnetic wave and travels at $3x10^8$ m/s

EM waves can be either visible or invisible according to their wavelength

Infrared thermograph --Introduction (2)

> b) Visible light frequency range Wave length (nm) Color 400-450 violet 450-480 blue 480-510 blue-green 510-550 green 550-570 yellow-green yellow 570-590 590-630 orange 630-700 red

Infrared thermograph --Introduction (3)

c) Invisible EM Waves

Wavelength λ < 0.4 μ m == ultraviolet
0.7 μ m < λ < 1.5 μ m == near-infrared
1.5 μ m < λ < 20 μm == mid-infrared

■ 20 μ m < λ == far infrared

Infrared thermograph --Introduction (4)

d) Infrared frequency range



Infrared thermograph --Mechanism (1)

Emission of EM waves by objects (The principle of blackbody radiation) Any object at non-zero temperature emits EM waves Infrared thermograph --Mechanism (2)

Infrared radiation and temperature related

- The wavelength of ITC is within the emission wavelength range of any object in the normal temperature range of -30°C to 100°C.
- Defects underneath can be detected by measuring the slight temperature fluctuation over the surface of an object.

Infrared thermograph -Active and passive measurements



Theoretical background for debonded tile detection (1)

$$B\frac{dT}{dt} = H - K(T - T_0)$$

- B Heat capacitance
- H Heat flow rate
- K Thermal conductivity

Initial condition: $t=0, T=T_0$

Theoretical background for debonded tile detection (2)

For heating process (H>0)

$$T = T_0 + \frac{H}{K} \left(1 - e^{-\frac{K}{B}t} \right)$$

■ For cooling process (H<0)

$$T = T_0 - \frac{\left|H\right|}{K} \left(1 - e^{-\frac{K}{B}t}\right)$$

Two Cases (1)

Two cases for voids between tile and substrate

- Case 1 = = voids are filled with water
- Case 2 = = Voids are empty (filled with air)

Two Cases (2)

Thermal Properties			
Material	Heat Capacity (J cm ⁻³ C ⁻¹)	Conductivity (W m ⁻¹ C ⁻¹)	
Air	0.0008	0.024	
Concrete	1.9	1	
Water	4.2	0.6	

Two Cases (3)

Case 1: Gap filled with water **During Heating proces** $T = T_0 + \frac{H}{K} \left(1 - e^{-\frac{K}{B}t} \right)$

	H/K	K/B
Concrete	Н	~1/1.9≈0.5
Water	1.6H	~1/7 ≈0.14

.: T is lower than concrete

During Cooling process
 T is higher than concrete

Two Cases (4)

Case 2: Gap filled with air **During Heating proces** $T = T_0 + \frac{H}{K} \left(1 - e^{-\frac{K}{B}t} \right)$

	H/K	K/B
Concrete	Н	~0.5
Water	42H	~ 30

... T is higher than concrete

During Cooling process T is lower than concrete

Two Cases (5)



- A debonded tile sample with half air and half water
- uniform heating of the inspected face
- after cooling for half an hour.





Thermal image of HKUST library indicating defected area filled with water on the external tiled walk





Thermograph of the government staff quarter under sunshine - indicating heavy damage on external wall

Reflection correction

$$N_{CAM} = \varepsilon N_{obj} + \rho N_{env}$$

where

 ε = object emissivity (the object is considered opaque)

 ρ = object reflectivity

 N_{obj} = radiance from the surface of the object

 N_{env} = radiance of the surrounding environment

Reflection correction

High emissivity case ($\varepsilon > 0.9$. $\varepsilon = (1-\rho)$) $N_{obj} \approx N_{CAM}$ Low emissivity case ($\varepsilon < 0.9$) Reflection should be considered Ceramic tile case ($\varepsilon = 0.6 - 0.8$) Reflection can not be neglected

Reflection correction


Reflection correction



Distance and angle --Space resolution

- Field view of an ITC depends on the lens of the system
- A camera may consist of 320 x 240 detectors in an array
- The area covered by each detector is the smallest size of an object
- Instantaneous field of view (IFOV)

Distance and angle - Space resolution

Example (20 degree by 15 degree lens)
Distance to object
IFOV

1m	0.35 x 0.26 m	1.1 x 1.1mm
5m	1.76 x 1.32 m	5.5 x 5.5mm
10m	3.52 x 2.63 m	11 x 11mm
50m	17.6 x 13.2 m	55 x 55mm

Influence on the area



Influence on radiation



Total received radiation

$A_0/\cos\alpha I_0 \cos\alpha = A_0 I_0$

Thumb rule for reality

- No [erfectly diffuse bodies exist
- For most bodies, the emissivity uually goes down from 50 degree from normal

Cement conduction mechanism



Conduction in cement is essentially electrolytic via ion transport through the interconnected pore network.

Traditional resistivity measurements





Non-contact resistivity measurement



Non-contact resistivity measurement





Procedures



Typical resistivity curve









microstructure formation process



Penetration method for setting time



Initial setting: Penetration resistance: 3.5 MPa

Final setting: Penetration resistance: 28 MPa (ASTM 403)





 $t_{fin} = 0.9202t_t + 0.2129$









Relationship between resistivity and strength



Relationship between water amount and lowest resistivity value



Dynamic modulus



Dynamic modulus



Results



Results



Results



Poison's ratio

$$v = A_{\rm l} \left(\frac{f_2}{f_1}\right)^2 + B_{\rm l} \left(\frac{f_2}{f_1}\right) + C_{\rm l} \quad (1)$$

where

$$A_{1} = -8.6457 \left(\frac{L}{D}\right)^{2} + 24.443 \left(\frac{L}{D}\right) - 12.478$$

$$B_{1} = 34.599 \left(\frac{L}{D}\right)^{2} - 101.72 \left(\frac{L}{D}\right) + 56.172$$
$$C_{1} = -34.681 \left(\frac{L}{D}\right)^{2} + 105.98 \left(\frac{L}{D}\right) - 62.731$$

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Poison's ratio



Dynamic modulus

$$E_{d} = 2(1+\nu)\rho \left(\frac{2\pi f_{1}R_{0}}{f_{n}^{1}}\right)^{2} \quad (2)$$

where

$$f_n^{-1} = A_2(\nu)^2 + B_2(\nu) + C_2 \qquad B_2 = 0.0846 \left(\frac{L}{D}\right)^2 - 0.5868 \left(\frac{L}{D}\right) + 1.3791$$
$$A_2 = -0.2792 \left(\frac{L}{D}\right)^2 + 1.4585 \left(\frac{L}{D}\right) - 2.1093 \qquad C_2 = 0.285 \left(\frac{L}{D}\right)^2 - 1.7026 \left(\frac{L}{D}\right) + 3.3769$$

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Dynamic Modulus



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Static and dynamic modulus








Cracking time of mortars with NaOH and KOH (w/c=0.45)





THE END

THANKS!